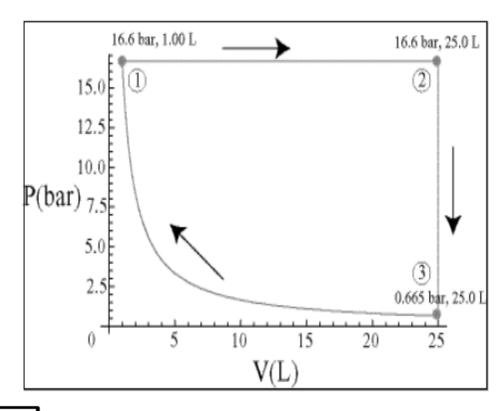
A system containing 2.50 mol of an ideal gas for which $C_V = 20.79 \ J \ mol^{-1}K^{-1}$ is taken through the cycle shown with the direction indicated by the arrows. The curved path corresponds to PV = nRT, where $T = T_1 = T_3$

Calculate q, w, and the changes in U and H for each segment, and for the cycle.



Path	ı	q	w	ΔU	ΔH
1→2	2	139.4 <i>kJ</i>	-39.8 k <i>J</i>	99.6 <i>kJ</i>	139.4 <i>kJ</i>
2→3	3	-99.6 kJ	0	-99.6 kJ	-139.4 <i>kJ</i>
3→1		-5.35 kJ	5.35 <i>kJ</i>	0	0
cycle	•	34.5 <i>kJ</i>	-34.5 <i>kJ</i>	0	0

From the Clapeyron equation derive an equation to express the vapor (saturation) pressure as a function of temperature. State your assumptions. The Clapeyron equation is given by:

$$\frac{dP^{sat}}{dT} = \frac{\Delta S^{lv}}{\Delta v^{lv}}$$

$$\Delta V \approx V^{gas}$$

$$\frac{dP}{dT} = \frac{\Delta S_m^{vaporization}}{\Delta V_m^{vaporization}} \approx \frac{\Delta H_m^{vaporization}}{TV^{gas}} = \frac{P\Delta H_m^{vaporization}}{RT^2}$$

$$\frac{dP}{P} = \frac{\Delta H_m^{vaporization}}{R} \frac{dT}{T^2}$$

$$\int_{P_i}^{P_f} \frac{dP}{P} = \frac{\Delta H_m^{vaporization}}{R} \int_{T_i}^{T_f} \frac{dT}{T^2}$$

$$\ln \frac{P_f}{P_i} = -\frac{\Delta H_m^{vaporization}}{R} \left(\frac{1}{T_f} - \frac{1}{T_i}\right)$$

Question 2 (continued)

The normal boiling temperature of benzene is $80.1^{\circ}C$, and the vapor pressure of liquid benzene is $10.4 \, kPa$ at $20.0^{\circ}C$. Calculate (a) ΔH (b) ΔS and (c) the percentage error between the value obtained in part (i) and the experimentally determined heat of vaporization

a) We can calculate $\Delta H_m^{vaporization}$ using the Clapyeron equation because we know the vapor pressure at two different temperatures

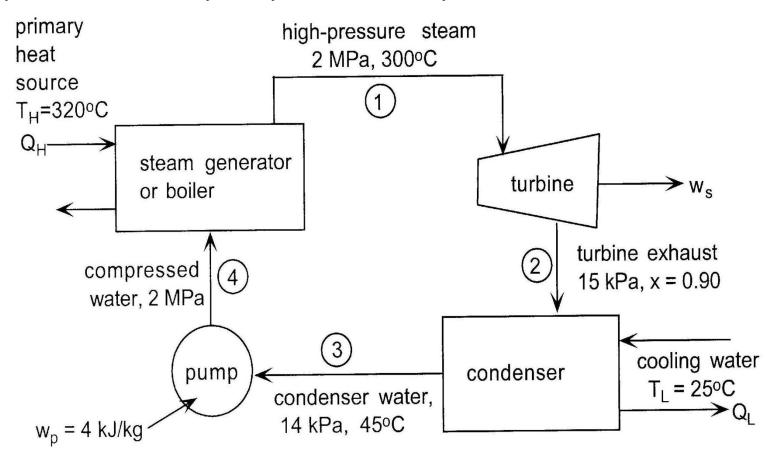
$$\begin{split} \ln \frac{P_f}{P_i} &= -\frac{\Delta H_m^{vaporization}}{R} \left(\frac{1}{T_f} - \frac{1}{T_i} \right) \\ \Delta H_m^{vaporization} &= -\frac{R \ln \frac{P_f}{P_i}}{\left(\frac{1}{T_f} - \frac{1}{T_i} \right)} = -\frac{8.314 J \, mol^{-1} K^{-1} \ln \frac{101325 Pa}{10000 Pa}}{\left(\frac{1}{273.15 + 80.09 K} - \frac{1}{273.15 + 20.0 K} \right)} \\ \Delta H_m^{vaporization} &= 33.2 k J \, mol^{-1} \end{split}$$

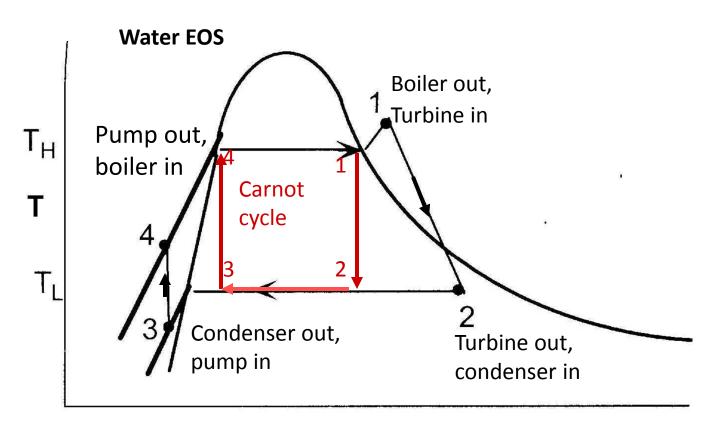
b)
$$\Delta S_m^{vaporization} = \frac{\Delta H_m^{vaporization}}{T_b} = \frac{33.2 \times 10^3 J \, mol^{-1}}{273.15 + 80.09 K} = 93.9 J \, mol^{-1} K^{-1}$$

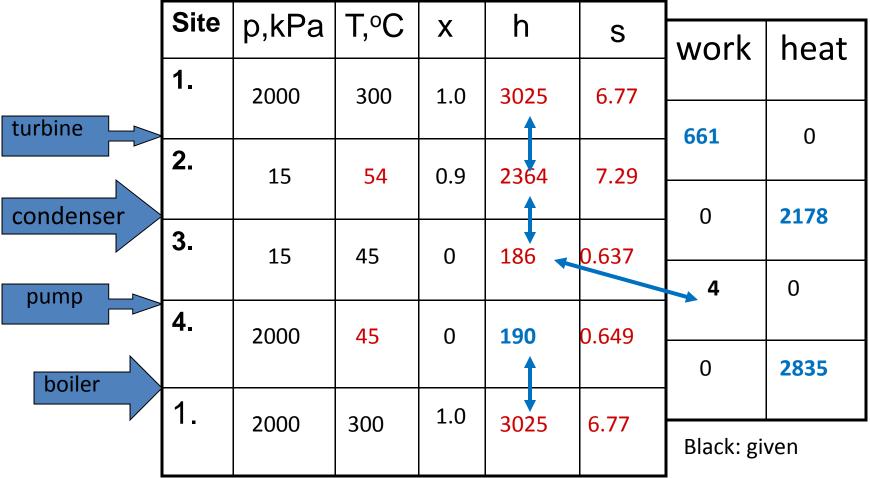
c) From Table B.2, $\Delta H^{Vaporiztion} = 30.72 \text{ kJ mol}^{-1}$ Therefore the error is 8.1%

For the power cycle shown below (assume 100% efficiency for the pump and turbine):

- Sketch the cycle on a *T-S* diagram.
- Calculate the work produced by the turbine.
- Calculate the change in entropy of the surroundings.
- Calculate the overall efficiency.
- If the rating of the cycle is 20.0 MW what is the steam flow rate?
- Is the cycle below realistic? If yes, why and if no, then why not?







red: STEAM TABLES

blue: 1ST law

- Work produced = 661 kJ/kg
- ΔS = entropy change of system (water/steam) in cycle

$$\Delta S = \Delta S_{turbine} + \Delta S_{condenser} + \Delta S_{pump} + \Delta S_{boiler}$$

$$= (7.29 - 6.77) + (0.64 - 7.29) + (0.65 - 0.64)$$

$$+ (6.77 - 0.65) = 0$$

$$\Delta S_{irr} = 0.649 - 0.637 + 7.29 - 6.77 = 0.53$$

$$(pump) \quad (turbine)$$

$$\Delta S_{surr} = Q_{condenser}/T_L + Q_{boiler}/T_H$$

$$= 2178/298 + (-2835)/593 = 2.52$$

$$\Delta S_{tot} = 0.53 + 2.52 = 3.05 \text{ kJ/Kg. K}$$

- Overall efficiency = (661 -4)/2835 = 0.23 = 23% (compared to 45% Carnot efficiency)
- Steam flow rate = 20,000/(661-4) = 30.4 kg/s

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(a) VdW:

V_{liq} = 161 \text{ cm}^3/\text{mol}

V_{vapour} = 4650 \text{ cm}^3/\text{mol}
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(b) PR:

V_{liq} = 95 \text{ cm}^3/\text{mol}
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 $V_{vapour} = 4087 \text{ cm}^3/\text{mol}$

Bonus

At the conditions specified (i.e. 5 bar and 320 K) Carbon Tetrachloride is a liquid because the vapour pressure (0.372 bar calculated from the Antoine equation, Table B.2) is lower than the operating pressure, and the normal boiling point temperature (349.8 K from table B.1 is higher than the operating temperature)